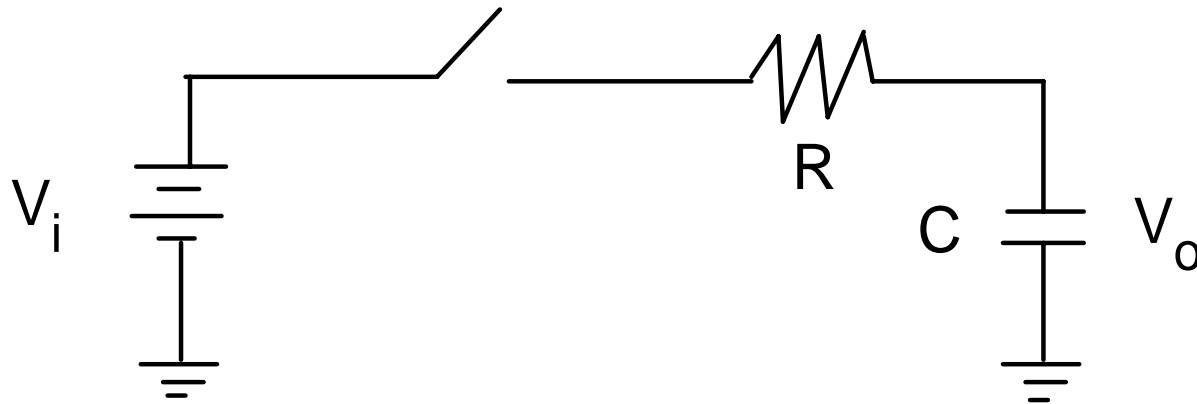


# **MEM 640 Lecture 1: Filters and Time Response**

# Filters: Why Study Them?

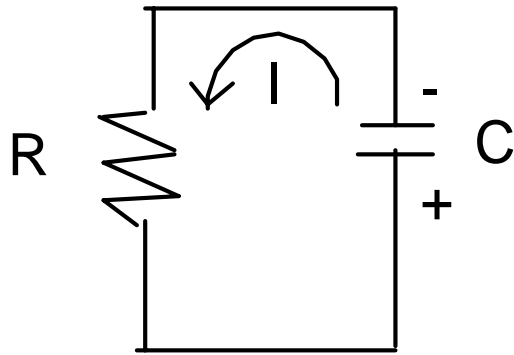


- Low Pass Filter is a classic first-order system
- Easily assembled for experimentation
- Differential equations are easy to derive: time domain
- Frequency domain easy to derive
- Show duality: time and frequency domain

# Background Math

**Case Study:** Calculate the voltage drop over a capacitor

Capacitor: sole purpose is to store electrons. Mechanical analog: reservoir tank



Recall

$$Q = CV$$

and

$$I = \frac{dQ}{dt} = C \frac{dV}{dt} + V \frac{dC}{dt} \quad (1)$$

Also, the cap is discharging across the resistor (hence negative):

$$I = -\frac{V}{R} \equiv C \frac{dV}{dt} \quad (2)$$

Equation (2) Is a differential equation and hence

$$\frac{dV}{dt} = -\frac{1}{RC} dt \quad (3)$$

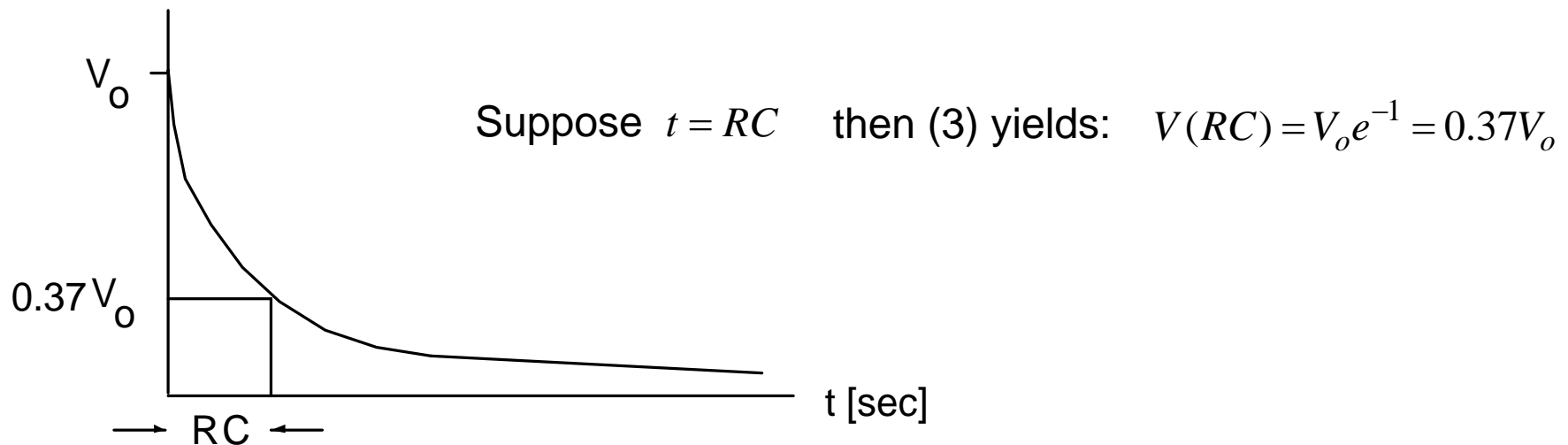
Integrating Equation (3) yields:

$$\ln V = -\frac{1}{RC}t + K_1 \quad \text{Where } K_1 \text{ is a constant}$$

Or

$$V(t) = e^{-t/RC} \cdot e^{K_1} = V_o e^{-t/RC} \quad \text{Where } V_o \text{ is a constant} \quad (4)$$

Plot of Equation (3) looks like:

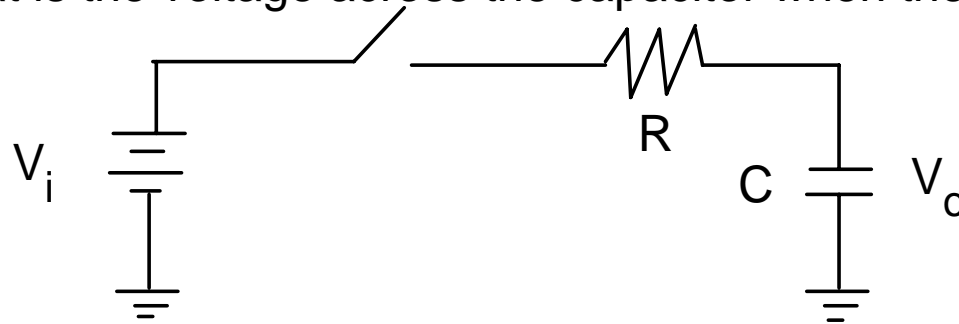


At  $V(3RC) = V_o e^{-3} = 0.05V_o$

Engineers call the 95% value 3 time constants

# Slightly Different Scenario

**Case Study:** What is the voltage across the capacitor when the switch is closed?



The equation for this circuit is:  $I = C \frac{dV_o}{dt} \equiv \frac{V_i - V_o}{R}$  where  $V_i$  is constant (5)

Then

$$\frac{dV_o}{dt} = \frac{1}{RC} (V_i - V_o) = \frac{V_i}{RC} - \frac{V_o}{RC} \quad (6)$$

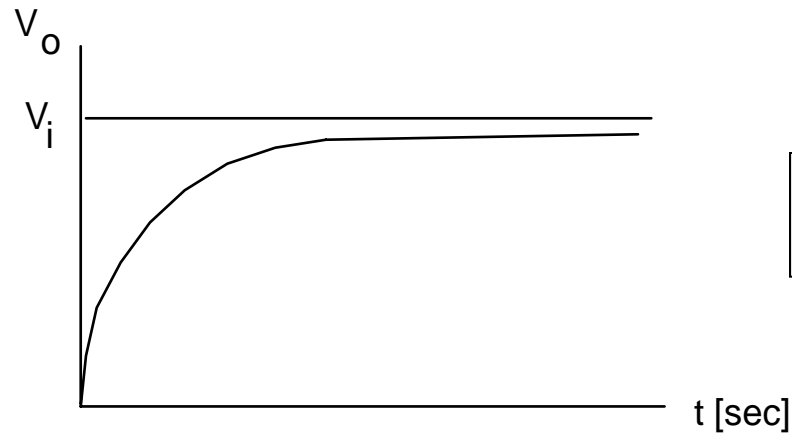
The solution to the non-homogeneous differential equation (6) is:

$$V_o(t) = V_i + A e^{-t/RC} \quad (7)$$

Given that  $V_o(0) = 0$  then  $A = -V_i$  and the solution to (7) becomes

$$V_o(t) = V_i(1 - e^{-t/RC}) \quad (8)$$

A plot of Equation (8) is



$$V_o(t) = V_i(1 - e^{-t/RC})$$

Note:

$$V(RC) = V_i(1 - e^{-1}) = 0.63V_i$$

and

$$V(5RC) = V_i(1 - e^{-5}) = 0.99V_i$$

A first order system reaches 99% of steady-state in 5 time constants. Also note that the plot of Equation (8) looks like ramp (in early part). That is why a low-pass filter is also known as an integrator

# Laplace Domain: Insights into Frequency Response

From (8) we derived the time response for a low pass filter as:

$$V_o(t) = V_i(1 - e^{-at}) \quad \text{where say } a = \frac{1}{RC} \quad (9)$$

Taking Laplace transform of (9) yields

$$V_o(s) = \frac{V_i}{s} - \frac{V_i}{s+a} = \frac{aV_i}{s(s+a)} \quad (10)$$

Now since  $V_i$  is a step input, recognize that

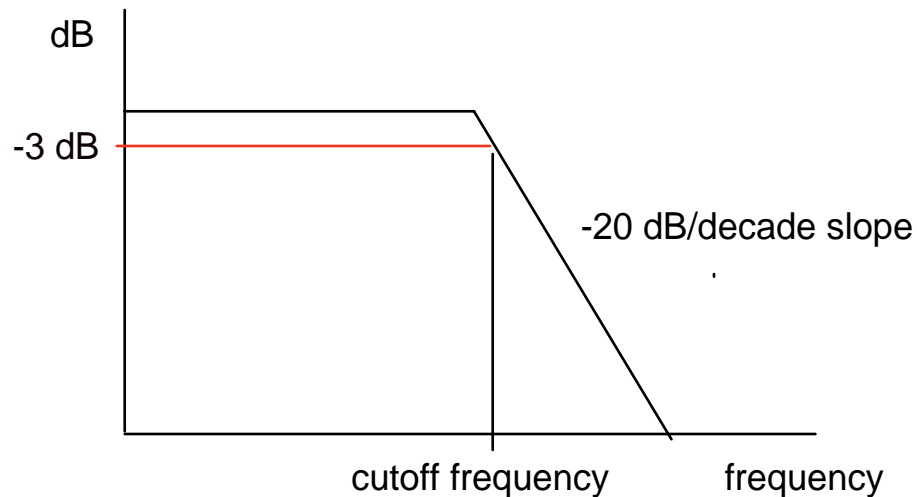
$$V_o(s) = \underbrace{\frac{a}{s+a}}_{\text{Actual transfer function}} \cdot \underbrace{\frac{V_i}{s}}_{\text{Step input contribution}}$$

Actual transfer function      Step input contribution

Thus transfer function for a low pass filter is given as

$$\boxed{\frac{V_o}{V_i} = \frac{a}{s+a}} \quad (11)$$

We will see later that the Bode Plot for (11) looks like



$$\frac{V_o}{V_i} = \frac{a}{s + a}$$

Recall that  $dB = 20 \log x$  thus at -3 dB we have  $x = 10^{-3/20} = 0.707$

Also recall from (8) that one time constant yields 63.3% of steady state

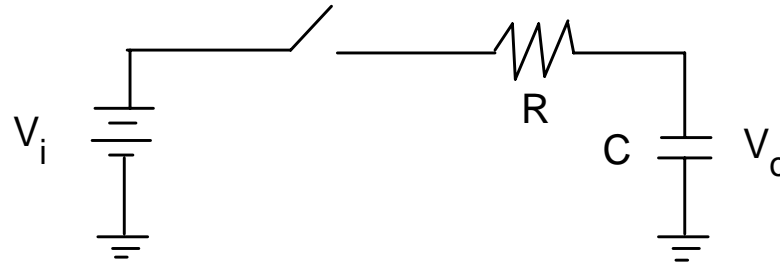
Thus the cutoff frequency is approximately the system's time constant value

$$\text{Also note that } (0.707)^2 = 0.499$$

Power is proportional to voltage squared. Hence the -3 dB point represents a 50% drop in power

# Where are we going with this?

**Problem:** Show mathematically, the integrative properties of the LP filter



**Solution:** The voltage across the resistor is  $V_i - V_o$  So:

$$I = C \frac{dV_o}{dt} \equiv \frac{V_i - V_o}{R} \quad (12)$$

Now suppose that  $V_o \ll V_i$  then (12) can be re-expressed as

$$C \frac{dV_o}{dt} \approx \frac{V_{in}}{R} \quad (13)$$

Or,

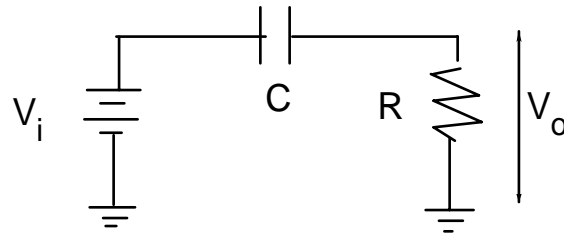
$$V_o(t) = \int \frac{V_{in}}{RC} dt = \frac{1}{RC} \int^t V_i(t) dt + \text{constant} \quad (14)$$

**Integration!**

The approximation (13) says the current is proportional to  $V_i$ . If  $V_i$  is large and  $R$  is large, then we have a current source.

# Hi Pass Filters Perform Derivatives

**Problem:** Show that a hi pass filter perform differentiation



**Solution:** The voltage across the cap is  $V_i - V_o$  so we have

$$I = C \frac{dV}{dt} = C \frac{d}{dt}(V_i - V_o) \equiv \frac{V_o}{R} \quad (15)$$

Now if  $R$  and  $C$  chosen small enough so that

$$\frac{dV_i}{dt} \gg \frac{dV_o}{dt} \quad (16)$$

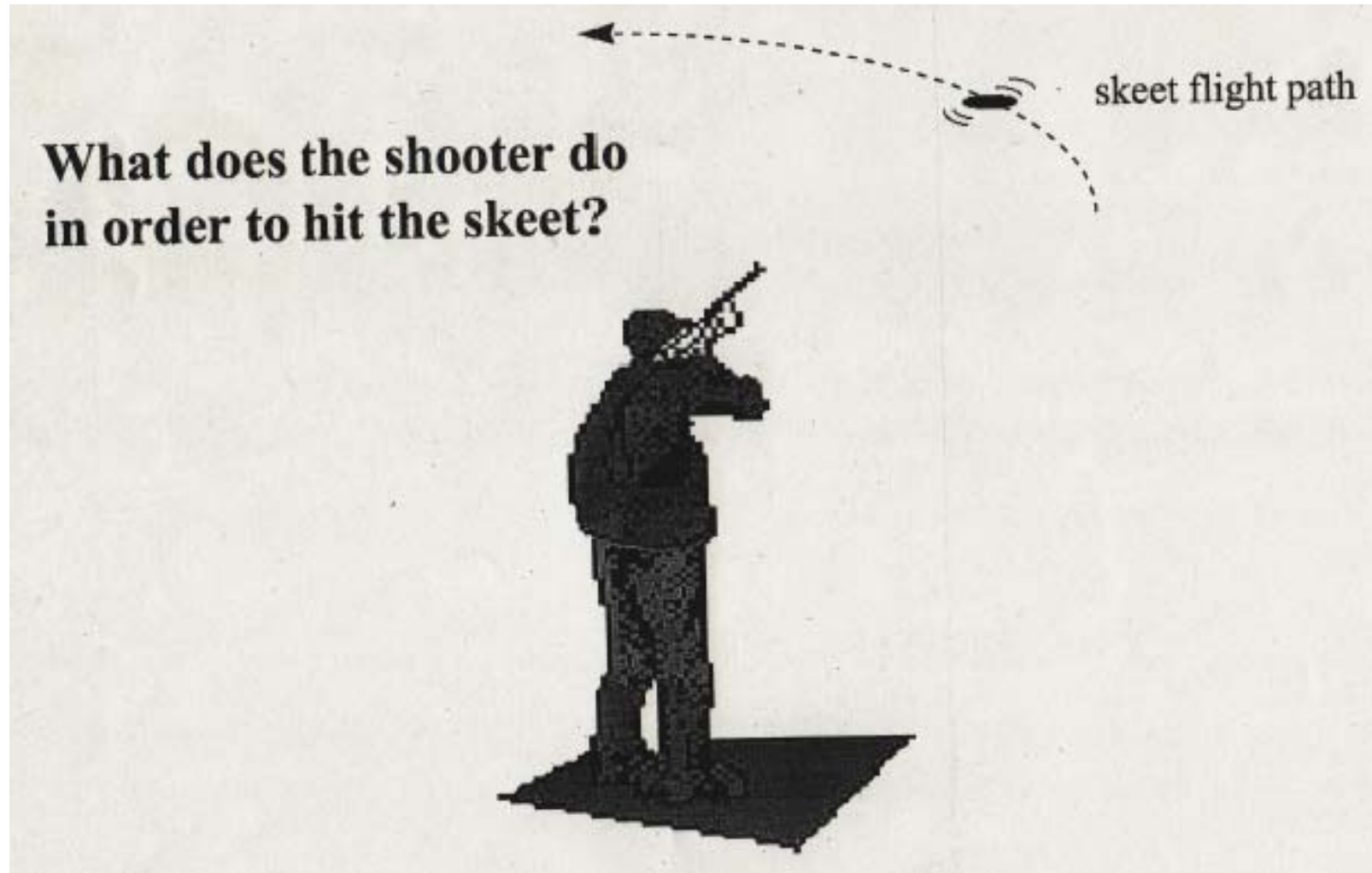
Then

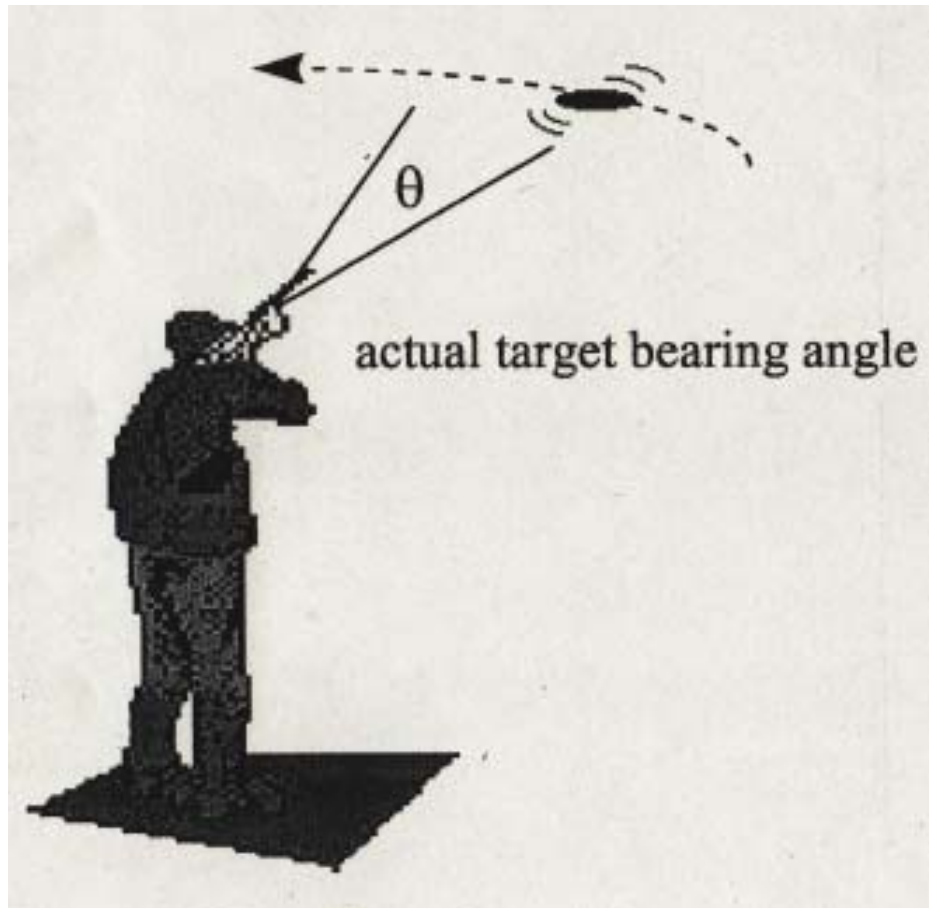
$$C \frac{dV_i}{dt} \approx \frac{V_o}{R} \quad (17)$$

Hence

$$V_o = \underbrace{RC}_{\text{Derivative!}} \frac{dV_i}{dt} \quad (18)$$

# Grandmother Explanation





Based on Target Dynamics

- Shooter adds angle theta
- Adds phase
- Shooter angle LEADS target angle
- Compensation
- Derivatives: rate of change
- Ignore high frequencies (hi-pass)

Differentiation  $\approx$  LEAD compensation  $\approx$  Hi-Pass Filter

